

**METHOD FOR GENERATING BROADBAND LIGHT SIDEBAND  
AND APPARATUS FOR GENERATING BROADBAND LIGHT  
SIDE BAND**

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**FIELD OF THE INVENTION**

[0001] The present invention relates to a method for generating a  
broadband light sideband and an apparatus for generating a broadband  
10 light sideband.

**BACKGROUND OF THE INVENTION**

[0002] As a method for generating a light sideband, a method using a  
mode-locked laser (MLL) and a method using an external phase  
modulator have been used so far. As a method using MLL, a method  
15 for generating a light sideband of a spectrum over two octaves using a  
nonlinear optical fiber is established. However, the light sideband  
sequence generated in this method has a small frequency interval of  
several hundred MHz, which is not sufficient in application for an  
optical communication system etc. Further, it is not easy to control  
20 the frequency interval of the light sideband sequence electrically. In  
addition, MLL being generally large and expensive, it is extremely  
hard to utilize it as a basic instrument applicable for the industrial  
base.

[0003] With a method using an external phase modulator, on the other  
25 hand, the frequency interval of the light sideband sequence can be  
made sufficiently large, for instance 10 GHz or more, and compact  
light sources of various kinds can advantageously be used. Further,  
the interval of the light sideband sequence can easily be controlled  
electrically. However, the amplitude of each sideband following the  
30 Bessel function, it is lacking in uniformity and there can happen that  
the sideband amplitude of a certain order is 0.

**DESCRIPTION OF THE PRESENT INVENTION**

**PROBLEMS TO BE SOLVED**

[0004] The present invention is intended for generating a light sideband sequence having a sufficiently large frequency interval, and each having a uniform intensity.

#### MEANS FOR SOLVING THE PROBLEMS

5 [0005] The present invention relates to a method for generating a broadband light sideband, comprises the steps of: inputting a light beam from a predetermined light source to an electro-optic phase modulator; generating a light sideband sequence by phase modulating the light beam in the electro-optic phase modulator; and making an  
10 intensity distribution of said light sideband sequence uniform by setting a predetermined spatial distribution of the phase modulation index within the beam cross-section in consideration with the spatial intensity distribution of said light beam.

[0006] Also, the present invention relates to an apparatus for  
15 generating a broadband light sideband, comprises: a predetermined light source; and an electro-optic phase modulator for generating a light sideband sequence by subjecting a phase modulation to a light beam emitted from said light source, and making an intensity distribution of said light sideband uniform by setting a predetermined  
20 spatial distribution of the phase modulation index in consideration with the spatial intensity distribution of said light beam.

[0007] According to the present invention, the frequency interval of the light sideband sequence can arbitrarily controlled based on the phase modulation frequency in the phase modulator with the use of the  
25 electro-optic phase modulator as an external phase modulator in generating the light sideband sequence. Thus, it is possible to increase the frequency interval of the light sideband sequence sufficiently by increasing the phase modulation frequency for instance to several GHz.

30 [0008] Moreover, in the electro-optic phase modulator, by setting a predetermined spatial distribution of phase modulation index in consideration with the spatial intensity distribution of the light beam used for generating the light sideband sequence and equalizing the

nonuniformity of the sideband generated in the phase modulation, it is possible to make the intensity distribution of the light sideband sequence uniform.

5 [0009] Therefore, according to the method of the present invention, a sufficient increase in the frequency interval in the intended light sideband sequence can be achieved, which is difficult with the conventional method using MLL and a nonlinear element, as well as the equalization of the intensity distribution of the light sideband sequence, which is impossible with the conventional method using the  
10 external phase modulator.

[0010] The spatial distribution of the phase modulation index is achieved by controlling the configuration of the electrode of the phase modulator in case, for example, the frequency of the modulation wave used for phase modulation is sufficiently low that a velocity  
15 mismatching between the light beam used for generating the light sideband sequence and the modulation wave is negligible in the electro-optic phase modulator. Specifically, the electrode is formed in such a way that the configuration thereof conforms with the configuration of the spatial distribution of the phase modulation index.

20 [0011] In addition, the electrode is installed on a pair of facing principal surfaces of the electro-optic crystal included in the electro-optic phase modulator, the surfaces extending generally parallel to the traveling direction of the light beam.

[0012] In case, on the other hand, the frequency used for phase  
25 modulation increases for example to several GHz and the velocity mismatching between the beam subjected to generation of the light sideband sequence and the modulation wave is not negligible in the electro-optic phase modulator, a quasi-velocity matching between the light beam and the modulation wave is obtained by applying a  
30 polarization reversal technique in the phase modulator.

[0013] In addition, the polarization reversal technique is applied to the electro-optic crystal included in the phase modulator. The electro-optic crystal is a main material comprising the majority of the phase

modulator.

[0014] By providing a means for spatial Fourier transformation in the backward of the electro-optic phase modulator, the light beam having been modulated in the light beam cross-section thereof by the electro-optic phase modulator with various modulation indices and comprising a sequence of light sidebands corresponding to each modulation index is added up using the spatial Fourier transformation. Thus, the intensity of the light beam comprising the light sideband sequence can always be kept constant.

10 [0015] An output means is appropriately provided to extract the output of the light beam in the backward of the electro-optic phase modulator, or of the spatial Fourier transformation means in case it is provided.

#### EFFECTS OF THE INVENTION

15 [0016] As described above, according to the present invention, the light sideband sequence can be generated with a sufficiently large frequency interval and a uniform intensity of each sideband.

#### BRIEF DESCRIPTION OF THE DRAWINGS

[0017] FIG. 1 is a configuration diagram illustrating schematically an example of an apparatus for generating a broadband light sideband according to the present invention.

FIG. 2 is a configuration diagram illustrating schematically another example of an apparatus for generating a broadband light sideband according to the present invention.

25 FIG. 3 is a configuration diagram illustrating schematically a modification example of an apparatus for generating a broadband light sideband as shown in FIG. 2.

FIG. 4 is a configuration diagram illustrating schematically another modification example of apparatus for generating a broadband light sideband as shown in FIG. 2.

#### 30 BEST MODE FOR CARRYING OUT THE INVENTION

[0018] A detailed description as well as other characteristics and advantages of the present invention is described below based on the best mode for carrying out the invention.

[0019] FIG. 1 is a configuration diagram illustrating schematically an example of an apparatus for generating a broadband light sideband according to the present invention. In an apparatus 10 shown in FIG. 1 for generating a sideband, a laser source 11, an electro-optic phase modulator 12 in the backward thereof and a light beam output means 13 are each provided in order of precedence. A high frequency power source 14 is further connected to an electro-optic phase modulator 12.

[0020] A light beam having a predetermined spatial distribution  $A(x)$  is emitted from the laser source 11 and introduced into the electro-optic phase modulator 12 to be modulated by a modulation wave generated in the high frequency power source 14 (a modulation wave is superimposed). In this process, a plurality of sidebands from a low order to a high order (a sideband sequence) are formed in the light beam.

[0021] In the conventional method, since the phase modulation index is constant over the whole beam, an uneven modulation sideband corresponding to the modulation index and similar to Bessel function is generated, so that there can happen that the sideband intensity of a specific index is almost zero. In the present invention, on the other hand, a spatial distribution  $g(x)$  of the phase modulation index is provided in the electro-optic phase modulator 12, sidebands of different modulation index are added up weightedly on account of spatial distribution  $A(x)$ , so that the intensity of a sideband sequence become uniform. As a result, a light sideband sequence of uniform intensity can be obtained.

[0022] When considering the spatial distribution  $g(x)$  of the phase modulation index, the phase of the light beam is modulated with the formula  $\psi(t, x) = g(x)\sin(2\pi f_m t)$ , wherein  $f_m$  represents the frequency of the modulation wave and  $t$  represents the time. Thus, the frequency of the light beam being  $f_0$ , the light beam is represented by formula 1, so that a sequence of sidebands lined up based on each modulation frequency is generated at position  $x$  at the output end of the crystal.



(Formula 1)

$$A(x)\exp[j (2\pi f_0 t - g(x) \sin(2\pi f_m t))]$$

$$= \sum_{n=-\infty}^{n=\infty} A(x)J_n(g(x))\exp[j (2\pi(f_0 - nf_m)t)]$$

The amplitude (intensity) of each sideband is represented by the  
 5 formula  $A(x)J_n(g(x))$ , the spatial distribution of the phase modulation  
 index  $g(x)$  is determined based on the above formula in such a way  
 that the amplitude (intensity) of each sideband corresponding to each  
 value  $n$  become constant.

[0023] In case the frequency of the modulation wave applied from the  
 10 high frequency power source 14 is relatively small and a velocity  
 mismatching with the light beam is negligible, desired spatial  
 distribution  $g(x)$  of the phase modulation index is obtained by  
 controlling the configuration of the electrode in the electro-optic phase  
 modulator 12. More specifically, the configuration of the electrode is  
 15 formed to be conformed with the configuration of spatial distribution  
 $g(x)$  of the phase modulation index. The electrode is installed on a  
 pair of facing principal surfaces of the electro-optic crystal included in  
 the electro-optic phase modulator, the surfaces extending generally  
 parallel to the traveling direction of the light beam,.

20 [0024] If the frequency of the modulation wave applied from the high  
 frequency power source 14 is relatively large, in an order of several  
 GHz for example, a polarization reversal technique is applied to the  
 electro-optic crystal included in the electro-optic phase modulator 12,  
 so that a crystal axis of the electro-optic crystal is reversed with  
 25 certain width  $W$  under the condition of a constant period.

[0025] Specifically, it is preferable to operate the polarization reversal  
 in the half-period of  $L=[2f_m(1/V_{gopt} - 1/V_{pmod})]^{-1}$ , wherein  $f_m$   
 represents the frequency of the modulation wave,  $V_{gopt}$  represents the  
 group velocity of the light beam and  $V_{pmod}$  represents the phase  
 30 velocity of the modulation wave. If the light beam has Gaussian  
 distribution for example, the spatial distribution of the modulated  
 index is represented by  $g(x) = 8nmL / \lambda \sin (\pi W (x) / (2L))$  having the  
 period of  $2L$ , wherein  $nm$  represents the change of the refraction index

caused by the impression of electric field on the electro-optic crystal,  $\lambda$  represents the wavelength of the light beam,  $L$  represents the period of the polarization reversal, and  $W(x)$  represents the polarization reversal width depending on the position  $x$ .

5 [0026] The electro-optic crystal is a main material comprising the majority of the electro-optic phase modulator 12.

[0027] FIG. 2 is a configuration diagram illustrating schematically another example of an apparatus for generating a broadband light sideband according to the present invention. An apparatus 20 for  
10 generating a broadband light sideband shown in FIG. 2 is different from the apparatus 10 for generating a broadband light sideband shown in FIG. 1 in that it comprises a convex lens 21 as a means to operate a spatial Fourier transformation behind the electro-optic phase modulator 12, a diffraction plate 22 provided with a slit 22A and an  
15 additional convex lens 23 behind the lens 21, while other elements are the same as in the apparatus 10 in FIG. 1. Thus, the phase modulation of the light beam emitted from laser source 11 can be operated in the same way to obtain the desired light sideband sequence. The diffraction plate 22 and the additional convex lens 23 are constituent  
20 of the output means for outputting the light beam.

[0028] The convex lens 21 is provided as a means for operating a spatial Fourier transformation in the backward of the electro-optic phase modulator 12. The light beam having been modulated in the cross-section thereof by the electro-optic phase modulator 12 with  
25 various modulation indices and comprising a sequence of light sidebands corresponding to each modulation index is added up by the convex lens 21 as a means for operating spatial Fourier transformation. The intensity of the light beam including the light sideband sequence can always be kept constant in this way.

30 [0029] The diffraction plate 22 is placed so that the slit 22A conforms with the focal point  $f$  of the convex lens 21. The light beam having passed through the convex lens 21 is narrowed by the slit 22A to be output via the additional convex lens 23.

[0030] A concave mirror can be substituted for the convex lens 23 as a means for operating a spatial Fourier transformation.

[0031] FIG. 3 is a configuration diagram illustrating schematically a modification example of an apparatus as shown in FIG. 2 for generating a broadband light sideband. In an apparatus 30 for generating a broadband light sideband as shown in FIG. 3, an optical fiber 31 is provided instead of the diffraction plate 22 and the additional convex lens 23 shown in FIG. 2 as an outputting means. The optical fiber 31 is provided in such a way that the input end thereof conforms with the focal point  $f$  of the convex lens 21 as a means for operating spatial Fourier transformation. In this case, a spatial Fourier transformation is operated with the convex lens 21 on the output light beam comprising the generated light sideband sequence, which is then introduced into the optical fiber 31 to be output.

[0032] FIG. 4 is a configuration diagram illustrating schematically another modification example of an apparatus as shown in FIG. 2 for generating a broadband light sideband. In an apparatus 40 as shown in FIG. 4 for generating a broadband light sideband, a diffraction grating 41 is provided instead of the diffraction plate 22 and the additional convex lens 23 in FIG. 2 as an outputting means. In this case, a spatial Fourier transformation is operated in convex lens 21 on the output light beam comprising the generated light sideband sequence, which is then diffracted with a diffraction grating 41 to be output.

[0033] While the present invention has been explained above in detail with some specific examples based on the mode for carrying out the invention, the invention is not to be considered as limited thereto, and various changes and modifications may be made without departing from the scope of the invention. For example, while the laser source is used in the above example, any light source can also be used instead. A light beam of any distribution configuration can be used by appropriately choosing a spatial distribution  $g(x)$  of the phase



modulation index.

[0034] In the same manner, while the intensity distribution of the light sideband sequence, for instance, is made uniform in the present invention, it is possible to generate a light sideband sequence of any  
5 intensity envelope besides the flat sideband distribution.

#### INDUSTRIAL APPLICABILITY

[0035] The present invention can be used in various fields such as optical electronics, optical information processing, optical communication, optical measurement and optical recording. More  
10 specifically, it can be applied to an optical frequency synthesizer, an optical pulse synthesizer, an optical frequency comb generator, an ultra short pulse generator and a light source for wavelength division multiplexing.